(54) Title: SINGLE MODE FIBRE
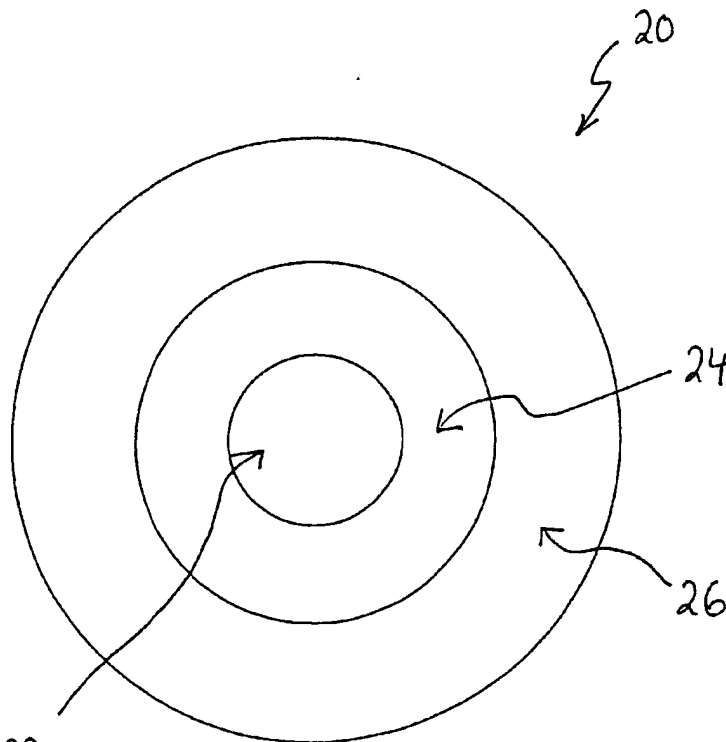
(57) Abstract: An optical fibre (20) is disclosed, the fibre is adapted in a manner such that it guides an optical signal substantially only in one non-degenerate mode, wherein an electro-magnetic field carrying the optical signal is symmetric with respect to rotation about the fibre axis. Preferably, the non-degenerate mode is the TE01 mode. In one embodiment, the optical fibre (20) includes a central hole region (22) surrounded by a concentric guiding region (24), which is in turn surrounded by a concentric cladding region 826). The guiding region (24) may comprise a Bragg reflector region. Through appropriate selection of design parameters of the fibre (20), the effective refractive index for the TM01 mode can be reduced relative to the TE01 mode to make it below a refractive index of the cladding region (269, resulting in leaking of the TM01 mode into the cladding region (26).

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Single M de Fibre

Field of the invention

The present invention relates broadly to an optical fibre and to a method of fabricating an optical fibre. The invention further relates to a device and method for generating an optical

5   signal for propagation in the optical fibre.

Background of the invention

Conventional "single" mode (SM) fibres are not true single mode fibres. This is because in conventional SM fibres the supported mode is the HE11 mode. The HE11 mode is 2 fold degenerate, corresponding to the two possible polarisations of the light wave in that mode.

10   Polarisation is a disadvantage in most applications of optical fibres, both in telecommunications and in sensing. In telecommunications, polarisation mode dispersion is one of the significant limiting factors encountered in data transmission in conventional SM fibres. In sensing employing interferometry, polarisation control must be exercised, or the sensitivity will fluctuate unpredictably, a form of "signal fading".

15   Single polarisation, single mode fibres have been proposed. In such designs the single polarisation, single mode characteristic is suggested to be achieved by choosing a strong asymmetric fibre design which causes the x and y modes to behave quite differently, one remaining guided and the other becoming lossy. However, one disadvantage of such designs is that fibre orientation needs to be considered when e.g. splicing fibres together, or in forming

20   fibre couplers or beam splitters.

In at least one of the preferred embodiments, the present invention seeks to provide a "true" single mode optical fibre for a light signal for which the modal field is substantially round, thereby e.g. eliminating the disadvantages associated with polarisation mode dispersion in data transport and signal fading in interferometry.

25   ## Summary of the invention

In accordance with a first aspect of the present invention there is provided an optical fibre adapted in a manner such that it guides an optical signal substantially only in one non-degenerate mode, wherein an electro-magnetic field carrying the optical signal is symmetric with respect to rotation about the fibre axis.

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Accordingly, the present invention can provide a single mode optical fibre eliminating the disadvantages associated with polarisation mode dispersion in data transport and signal fading in interferometry, and having the advantage of not needing to consider fibre orientation when e.g. splicing fibres together or in forming fibre coupler or beam splitters.

5   Preferably, the non-degenerate mode is the TE01 mode.

In one embodiment, the optical fibre comprises a central hole region along its length symmetric with respect to rotation about the fibre axis, a concentric guiding region symmetric with respect to rotation about the fibre axis around the hole region, and a cladding region around the guiding region, wherein the diameter of the hole region, the thickness of the guiding

10   region, the refractive index of the guiding region, and the refractive index of the cladding region are chosen such that, in use, only the one non-degenerate mode is guided in the guiding region.

Preferably, the diameter of the hole region, the thickness of the guiding region, the refractive index of the guiding region, and the refractive index of the cladding region are chosen such that, in use, an effective refractive index for the HE11 mode of the optical signal is

15   reduced to be equal to or below the refractive index of the cladding region, whereby the HE11 mode is radiated away from the guiding region.

The refractive index of the guiding region and/or the cladding region may be graded.

In an alternative embodiment, the optical fibre comprises a concentric Bragg reflector region symmetric with respect to rotation about the fibre axis around a guiding region

20   symmetric with respect to rotation about the fibre axis, wherein the Bragg reflector region is arranged in a manner such that, in use, least leaking into the cladding region is experienced by the TE01 mode, whereby substantially only the TE01 mode is guided in the guiding region.

The optical fibre in such an embodiment may comprise a photonic crystal fibre.

The optical fibre in such an embodiment may further comprise a central hole region

25   symmetric with respect to rotation about the fibre axis arranged in a manner such that an effective refractive index for the HE11 mode of the optical signal is reduced to be equal to or below the refractive index of the cladding region, whereby the HE11 mode is radiated away from the guiding region to assist suppressing guiding of the HE11 mode in the guiding region.

In yet another alternative embodiment, the optical fibre may comprise absorption means

30   adapted to preferentially absorb light in modes other than the one non-degenerate mode. The

optical fibre in such an embodiment may further comprise amplifying means adapted to amplify substantially only the one non-degenerate mode. The absorption means and/or the amplification means may comprise regions of the optical fibre made from a suitable optically absorbing or amplifying material respectively.

5   In accordance with a second aspect of the present invention there is provided a method of manufacturing an optical fibre, the method comprising the step of selecting design parameters in the manufacture of the optical fibre in a manner such that the optical fibre guides an optical signal only in one non-degenerate mode, wherein an electro-magnetic field carrying the optical signal is symmetric with respect to rotation about the fibre axis.

10   Preferably, the non-degenerate mode is the TE01 mode.

In one embodiment, the method comprises the step of selecting the diameter of a central hole region symmetric with respect to rotation about the fibre axis, the thickness of a concentric guiding region symmetric with respect to rotation about the fibre axis around the hole region, the refractive index of the guiding region, and the refractive index of a cladding region of the

15   fibre around the guiding region such that, in use, only the one non-degenerate mode is guided in the guiding region.

Preferably, the diameter of the hole region, the thickness of the guiding region, the refractive index of the guiding region, and the refractive index of the cladding region are selected such that, in use, an effective refractive index for the HE11 mode of the optical signal

20   is reduced to be equal to or below the refractive index of the cladding region, whereby the HE11 mode is radiated away from the guiding region.

The refractive index of the guiding region and/or the cladding region may be graded.

In an alternative embodiment, the method comprises the steps of selecting a Bragg reflector region symmetric with respect to rotation about the fibre axis around a guiding region

25   symmetric with respect to rotation about the fibre axis and arranged in a manner such that, in use, least leaking into a cladding region of the fibre around the Bragg region is experienced, in use, by the TE01 mode, whereby substantially only the TE01 mode is guided in the guiding region.

The optical fibre in such an embodiment may comprise a photonic crystal fibre.

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The method in such an embodiment may further comprise the step of forming a central hole region in the optical fibre symmetric with respect to rotation about the fibre axis and arranged in a manner such that an effective refractive index for the HE11 mode of the optical signal is reduced to be equal to or below the refractive index of the cladding, whereby the HE11 mode is radiated away from the guiding region to assist suppressing guiding of the HE11 mode in the guiding region.

The method in yet another alternative embodiment may comprise the steps of providing absorption means associated with the optical fibre and adapted to preferentially absorb light in modes other than the one non-degenerate mode. The method in such an embodiment may further comprise the step of providing amplifying means associated with the optical fibre and adapted to amplify substantially only the one non-degenerate mode. The absorption means and/or the amplification means may comprise regions of the optical fibre made from a suitable optically absorbing or amplifying material respectively.

In accordance with a third aspect of the present invention there is provided a light source structure adapted in a manner such that it generates a light signal which comprises substantially only one non-degenerate mode, wherein a modal field of the light signal is substantially round.

Preferably, the light source structure comprises an optical fibre laser, wherein the optical fibre laser comprises an optical fibre as defined in the first aspect of the present invention.

In accordance with a fourth aspect of the present invention there is provided a method of generating a light signal which comprises substantially only one non-degenerate mode, and wherein a modal field of the light signal is substantially round.

Preferably, the method comprises the step of effecting lasing to occur in an optical light source structure as defined in the third aspect of the present invention.

Brief description of the drawings

Preferred forms of the present invention will now be described, by way of example only, with reference to the accompanying drawings.

Figure 1 shows a plot of the intensity of different modes of propagation of an optical signal travelling in a typical radially symmetric waveguide as a function of radius r.

Figure 2 is a schematic cross sectional view of an optical fibre embodying the present invention.

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Figure 3 is a schematic cross sectional view of another optical fibre embodying the present invention.

Figure 4 is a schematic cross sectional view of another optical fibre embodying the present invention.

5   Figure 5 is a schematic cross sectional view of another optical fibre embodying the present invention.

Figures 6(A), (B) & (C) are schematic diagrams illustrating a manufacturing process for an optical fibre embodying the present invention.

Figure 7 is a schematic diagram illustrating an optical fibre laser arrangement

10   embodying the present invention.

Detailed description of the embodiments

The preferred embodiments described provide an optical fibre adapted in a manner such that it guides an optical signal substantially only one non-degenerate mode, and wherein a modal field of the guided light signal is substantially round. The preferred embodiments

15   described have the advantage that there is no need to select the fibre orientation in splicing fibres together, or forming structures such as fibre couplers or beam splitters.

Figure 1 shows a plot of the intensity of different modes of propagation of an optical signal travelling in a radially symmetric waveguide as the function of the radius r. As can be seen from Figure 1 the intensity curve for the highest mode HE11, curve 10, has a maximum at

20   the centre of the waveguide. In contrast, the curve for what is normally the next lower mode, the TE01 mode, curve 12, has its maximum intensity in a doughnut shaped maximum around the centre of the waveguide. Importantly, the TE01 mode is a non-degenerate mode. That is, in this mode the magnetic quantum number m = 0. Thus a light signal that propagates only in e.g. the TE01 mode will not experience polarisation mode dispersion or interferometric signal

25   fading resulting from superposition of polarisations.

In one embodiment of the present invention illustrated in Figure 2, an optical fibre 20 is designed having the following characteristics. It comprises a central hole region 22, surrounded by a concentric guiding region 24, which is in turn surrounded by a concentric cladding region 26.

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It is the design object in the optical fibre 20 to chose the design parameters in a manner such that the effective refractive index for the HE11 mode is reduced due to the presence of the hole region 22 to a value equal to or below the refractive index of the cladding region 26. If this design condition is achieved, the HE11 mode will be leaking from the guiding region 24

5   through the cladding region 26, i.e. its guided propagation along the guiding region 24 of the optical fibre 20 is suppressed.

It will be appreciated by a person skilled in the art, that through appropriate selection of the design parameters of the optical fibre 20, the presence of the hole region 22 will not significantly perturb the TE01 mode (compare Figure 2) thus leaving the TE01 mode as the

10 mode with the now highest effective refractive index experienced by any mode. Through suitable selection of the design parameters of the optical fibre 20 in the exemplary embodiment such that the effective refractive index experienced by all other (lower) modes will be equal to or lower than the refractive index of the cladding region 26, those modes will also leak from the guiding region 24.

15 Depending on the material and/or wavelength of a light signal of interest, the effective refractive index for the TM01 mode can be close to the effective refractive index for the TE01 mode. It may then be advantageous to provide a further means for assisting the suppression of light propagation in the TM01 mode. In another optical fibre design 100 embodying the present invention shown in Figure 3, closely spaced concentric rings e.g. 102, 104 of alternating

20 refractive index are placed within a concentric guiding region 106 roughly where the TE01 mode (and the TM01 mode) has a maximum intensity (compare Figure 1). The fibre design 100 further comprises a central hole region 108 and a concentric cladding region 110.

In the fibre design 100, the concentric rings e.g. 102, 104 of alternating refractive index is expected, in an example embodiment, to alter the effective refractive index for the TE01

25 mode more than for the TM01 mode. Through appropriate selection of the design parameters, the effective refractive index for the TM01 mode can be reduced relative to the TE01 mode to assist in ensuring that it is equal to or below the refractive index of the cladding region 110, which in turn ensures that the TM01 mode experiences leaking into the cladding region 110.

In yet another embodiment of the present invention shown in Figure 4, an optical fibre

30 50 comprises a cylindrical centre region 52 surrounded by a concentric guiding region 54, which in turn is surrounded by a concentric cladding region 56.

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The material of which the central region 52 is formed is chosen such that it absorbs light at the wavelength of a particular light signal intended for propagation in the guiding region 54.

It will be appreciated by the person skilled in the art that, since the HE11 mode has a maximum in its intensity at the centre of the optical fibre 50 (compare Figure 1), this will result

5   in preferential absorption of the HE11 mode. This is in contrast with the situation for the TE01 mode (compare Figure 1), which will experience an insignificant perturbance caused by the absorption in the centre region 52, provided that the design parameters of the optical fibre 50 are chosen appropriately.

In a modification of the optical fibre 50 shown in Figure 4, the material of the guiding

10   region 54 may further be chosen in a manner such that it amplifies light at the wavelength of the particular light signal, which will in effect result in preferential amplification of the TE01 mode, which has a doughnut shape maximum in its intensity in the area of the guiding region 54 (compare Figure 1) if the design parameters chosen appropriately. This can enhance the true single mode characteristics of an optical fibre embodying the present invention.

15   In a preferred embodiment of the present invention shown in Figure 5, an optical fibre 40 comprises a core region 42, surrounded by a concentric Bragg reflector region 44, which in turn is surrounded by a concentric cladding region 46. The Bragg reflector region 44 comprises a refractive index profile, in an exemplary embodiment symmetric with respect to rotation about the fibre axis, which constitutes a grating structure with respects to a light signal propagated

20   within the core region 42.

In the preferred embodiment, the set of concentric Bragg reflecting layers of successive higher and lower refractive index, e.g. 43, 45 can be made more effective in the preferential guidance of the TE polarised modes by choosing its parameters so that its reflectivity is polarisation dependent. The phenomena connected with the Brewster angle in a planar stack of

25   layers of alternating refractive index n_1 and n_2 has been found to have an analogue for a similar concentric stack in the Bragg fibre 40. For a given wavelength and alternating indices n_1 and n_2 the effective refractive index of the best guided mode can be adjusted quite freely by varying the thickness of the layers e.g. 43, 45 (and so the Bragg condition) and the size of the core 42. The Brewster condition for a planar stack coincides with that for a Bragg fibre at large radius and

30   may be written $n_{\text{eff}} = n_1 n_2 / \sqrt{n_1^2 + n_2^2}$, where n_{eff} is the effective refractive index at the

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given wavelength. For values of n_{eff} in a Bragg fibre close to meeting this Brewster condition, i.e. embodying the present invention, Bragg reflection is undermined for TM modes and also for hybrid modes, which have a component of TM polarisation.

5   It has been found by the applicant that in the optical fibres of the design of optical fibre 40 shown in Figure 5, the least leaking of light intensity occurs for the TE01 mode. In other words, the optical fibre 40 of the preferred embodiment will preferentially guide light only in the TE01 mode, whilst suppressing the guiding of any of the other modes. It will be appreciated that for the fibre to be effectively single moded, there must be a sufficient difference between the losses of the best guided mode and of the other modes. At the same time, the loss of the best
10   guided mode should be low enough that the fibre can be used for transmission. These considerations lead to the concept of a length L_{sm} beyond which the fibre is effectively single moded, and a maximum useful length L_{max}.

Table I shows results of calculations conducted on an example design of optical fibre 40. In that example design, an air core region 42 (refractive index n=1) of radius 1.828μm, and 16
15   pairs of high and low refractive index layers e.g. 43, 45 respectively where considered. The refractive index of the high index layer e.g. 43 is 1.49, thickness 0.2133μm, and the refractive index of the lower index layer e.g. 45 is 1.17, thickness 0.346μm.

Table I displays the loss in dB/m for each mode. The second last column shows the length in metres $L_{1\%}$, at which the transmitted power in that mode is reduced to 1%. The last
20   column is the length $L_{0.01\%} = 2L_{1\%}$, at which the power in that mode is reduced to 0.01%. From the figures in the last two columns it can be illustrated in the example embodiment at what minimum length ($L_{sm}=L_{.01\%}$ for second best guided mode) the fibre is effectively single moded, and what the maximum useful length is ($L_{max}=L_{1\%}$ for best guided mode). In other words, for illustrative purposes the example fibre is substantially single moded for length greater than
25   about $L_{sm}=2cm$, and is usefully transmissive up to a length of $L_{max}=400m$. Whilst for this illustration only the second best guided mode was taken into account in determining the onset of single modedness, it will be appreciated that it does not make much difference if other modes of lower loss are also taken into account. Modes omitted from Table I are lossier than those shown. Furthermore, it will be appreciated that the results shown in Table I are illustrative only
30   of an example embodiment of the present invention, and that the present invention is not limited to such a design.

mode class		effective index (β/k)		loss (dB/m)	$L_{1\%}$ m (20dB)	$L_{0.01\%}$m (40dB)
m*		real	imaginary			
0	TE	0.941762	9.2086×10^{-10}	5.026×10^{-2}	398	796
0	TE	0.812685	3.1489×10^{-5}	1.719×10^{3}	1.16×10^{-2}	2.33×10^{-2}
1	hybrid	0.888962	1.3357×10^{-3}	7.290×10^{4}	2.74×10^{-4}	5.49×10^{-4}
0	TE	0.789125	2.278×10^{-3}	1.243×10^{5}	1.61×10^{-4}	3.22×10^{-4}
1	hybrid	0.977576	2.408×10^{-3}	1.314×10^{5}	1.52×10^{-4}	3.04×10^{-4}
2	hybrid	0.82833	2.957×10^{-3}	1.614×10^{5}	1.24×10^{-4}	2.48×10^{-4}
3	hybrid	0.765984	5.137×10^{-3}	2.804×10^{5}	7.13×10^{-5}	1.43×10^{-4}

* The azimuthal field dependence is $\exp(\pm im\varphi)$

Table I

It will be appreciated by a person skilled in the art that the optical fibres of the exemplary embodiments can be manufactured utilising existing optical fibre manufacturing techniques. One exemplary method of manufacturing the optical fibre 20 (see Figure 2) embodying the present invention will now be described briefly with reference to Figure 6. In Figure 6A, as a first step a preform 30 is manufactured utilising known techniques such as modified chemical vapour deposition (MCVD) inside a tubular carrier member (not shown). The preform 30 has a step function in its refractive index i.e. it consists on a core region 32 and a cladding region 34 of differing refractive index.

As shown in Figure 6B, in a next step a hole 36 is created in the preform 30 through e.g. drilling.

In a final step shown in Figure 6C, an optical fibre 38 is drawn from the preform 30. It will be appreciated by a person skilled in the art that the design parameters of the preform 30 can be selected such that they correspond to the desired design characteristics of the optical fibre 20.

In an alternative embodiment, a method of manufacturing an optical fibre of the type of optical fibre 40 (see Figure 5) comprises utilising glass for the high index rings and glass with

holes for the lower index rings and core, to achieve a desired refractive index contrast. Such structures form a sub-set of what are referred to as "photonic crystal" or "holey" fibres.

Figure 7 shows an optical fibre laser signal arrangement 60 embodying the present invention. The optical fibre laser arrangement 60 comprises a pump laser source 62 for pumping

5   an optical fibre laser 64. Importantly, the optical fibre laser 64 comprises an optical fibre embodying the present invention, in the exemplary embodiment an optical fibre of the type of optical fibre 40 described above with reference to Figure 5.

It will be appreciated by the person skilled that to construct the fibre laser 64 utilising an optical fibre of the type of optical fibre 20, e.g. a suitable dopant material is provided in the

10   guiding region 24 (see Figure 2) to effect lasing between reflective elements 66, 68 at end portions of the optical fibre laser 64. One of the reflective elements 66 is e.g., a semi-transparent reflective element, thus enabling emission of the TE01 laser beam 70.

It will be appreciated by a person skilled in the art that the optical fibre laser arrangement 60 is suitable for substantially direct coupling of light into optical fibre embodying

15   the present invention, e.g., optical fibre of the type of optical fibre 20, optical fibre 100, or optical fibre 50 described above with reference to Figure 2, Figure 3, and Figure 6 respectively.

It will be appreciated by the person skilled in the art that numerous modification and/or variations may be made to the present invention as shown in the specific embodiments without departing from the spirit or scope of the invention as broadly described.   The present

20   embodiments are, therefore, to be considered in all respects to be illustrative and not restrictive.

In the claims that follow and in the summary of the invention, except where the context requires otherwise due to express language or necessary implication the word "comprising" is used in the sense of "including", i.e. the features specified may be associated with further features in various embodiments of the invention.

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Claims

1.   An optical fibre adapted in a manner such that it guides an optical signal substantially only in one non-degenerate mode, wherein an electro-magnetic field carrying the optical signal is symmetric with respect to rotation about the fibre axis.

5   2.   An optical fibre as claimed in claim 1, wherein the non-degenerate mode is the TE01 mode.

3.   An optical fibre as claimed in claim 1, wherein the optical fibre comprises:

- a central hole region along its length symmetric with respect to rotation about the fibre axis,

10   - a concentric guiding region symmetric with respect to rotation about the fibre axis around the hole region, and

- a cladding region around the guiding region,

wherein the diameter of the hole region, the thickness of the guiding region, the refractive index of the guiding region, and the refractive index of the cladding region are chosen

15   such that, in use, only the one non-degenerate mode is guided in the guiding region.

4.   An optical fibre as claimed in claim 3, wherein the diameter of the hole region, the thickness of the guiding region, the refractive index of the guiding region, and the refractive index of the cladding region are chosen such that, in use, an effective refractive index for the HE11 mode of the optical signal is reduced to be equal to or below the refractive index of the

20   cladding region, whereby the HE11 mode is radiated away from the guiding region.

5.   An optical fibre as claimed in claim 3, wherein the refractive index of the guiding region and/or the cladding region is graded.

6.   An optical fibre as claimed in claim 1, wherein the optical fibre comprises:

- a concentric Bragg reflector region symmetric with respect to rotation about the fibre

25   axis around a guiding region symmetric with respect to rotation about the fibre axis,

wherein the Bragg reflector region is arranged in a manner such that, in use, least leaking into the cladding region is experienced by the TE01 mode, whereby substantially only the TE01 mode is guided in the guiding region.

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7.   An optical fibre as claimed in claim 6, wherein the optical fibre comprises a photonic crystal fibre.

8.   An optical fibre as claimed in claim 6, wherein the optical fibre further comprises a central hole region symmetric with respect to rotation about the fibre axis arranged in a manner such that an effective refractive index for the HE11 mode of the optical signal is reduced to be equal to or below the refractive index of the cladding region, whereby the HE11 mode is radiated away from the guiding region to assist suppressing guiding of the HE11 mode in the guiding region.

9.   An optical fibre as claimed in claim 1, wherein the optical fibre comprises:

- absorption means adapted to preferentially absorb light in modes other than the one non-degenerate mode.

10.   An optical fibre as claimed in claim 9, wherein the optical fibre further comprises amplifying means adapted to amplify substantially only the one non-degenerate mode.

11.   An optical fibre as claimed in claim 9, wherein the absorption means and/or an amplification means comprise regions of the optical fibre made from a suitable optically absorbing or amplifying material respectively.

12.   A method of manufacturing an optical fibre, the method comprising the step of selecting design parameters in the manufacture of the optical fibre in a manner such that the optical fibre guides an optical signal substantially only in one non-degenerate mode, wherein an electro-magnetic field carrying the optical signal is symmetric with respect to rotation about the fibre axis.

13.   A method as claimed in claim 12, wherein the non-degenerate mode is the TE01 mode.

14.   A method as claimed in claim 12, wherein the method comprises the step of:

- selecting the diameter of a central hole region symmetric with respect to rotation about the fibre axis, the thickness of a concentric guiding region symmetric with respect to rotation about the fibre axis around the hole region, the refractive index of the guiding region, and the refractive index of a cladding region of the fibre around the guiding region such that, in use, only the one non-degenerate mode is guided in the guiding region.

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15.   A method as claimed in claim 14, the diameter of the hole region, the thickness of the guiding region, the refractive index of the guiding region, and the refractive index of the cladding region are selected such that, in use, an effective refractive index for the HE11 mode of the optical signal is reduced to be equal to or below the refractive index of the cladding

5   region, whereby the HE11 mode is radiated away from the guiding region.

16.   A method as claimed in claim 14, wherein the refractive index of the guiding region and/or the cladding region is graded.

17.   A method as claimed in claim 12, wherein the method comprises the steps of:

- selecting a Bragg reflector region symmetric with respect to rotation about the fibre

10   axis around a guiding region symmetric with respect to rotation about the fibre axis and arranged in a manner such that, in use, least leaking into a cladding region of the fibre around the Bragg region is experienced, in use, by the TE01 mode, whereby substantially only the TE01 mode is guided in the guiding region.

18.   A method as claimed in claim 17, wherein the optical fibre comprises a photonic

15   crystal fibre.

19.   A method as claimed in claim 17, wherein the method further comprises the step of:

- forming a central hole region symmetric with respect to rotation about the fibre axis in the optical fibre and arranged in a manner such that an effective refractive index for the HE11

20   mode of the optical signal is reduced to be equal to or below the refractive index of the cladding, whereby the HE11 mode is radiated away from the guiding region to assist suppressing guiding of the HE11 mode in the guiding region.

20.   A method as claimed in claim 12, wherein the method comprises the steps of providing absorption means associated with the optical fibre and adapted to preferentially

25   absorb light in modes other than the one non-degenerate mode.

21.   A method as claimed in claim 20, wherein the method further comprises the step of providing amplifying means associated with the optical fibre and adapted to amplify substantially only the one non-degenerate mode.

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22. A method as claimed in claim 20, wherein the absorption means and/or an amplification means comprise regions of the optical fibre made from a suitable optically absorbing or amplifying material respectively.

23. A light source structure adapted in a manner such that it generates a light signal which comprises substantially only one non-degenerate mode, wherein a modal field of the light signal is substantially round.

24. A light source structure as claimed in claim 23, wherein the light source structure comprises an optical fibre laser, and wherein the optical fibre laser comprises an optical fibre as defined in any one of claims 1 to 11.

25. A method of generating a light signal which comprises substantially only one non-degenerate mode, wherein a modal field of the light signal is substantially round.

26. A method as claimed in claim 25, wherein the method comprises the step of effecting lasing to occur in an optical light source structure as defined in claims 23 or 24.

Figure 1

20

24

26

22
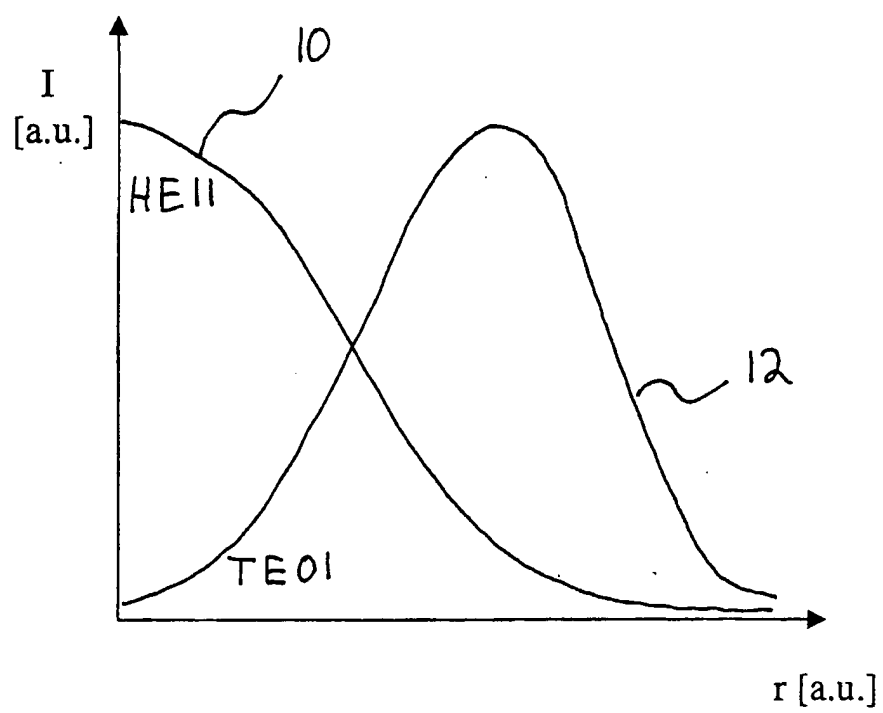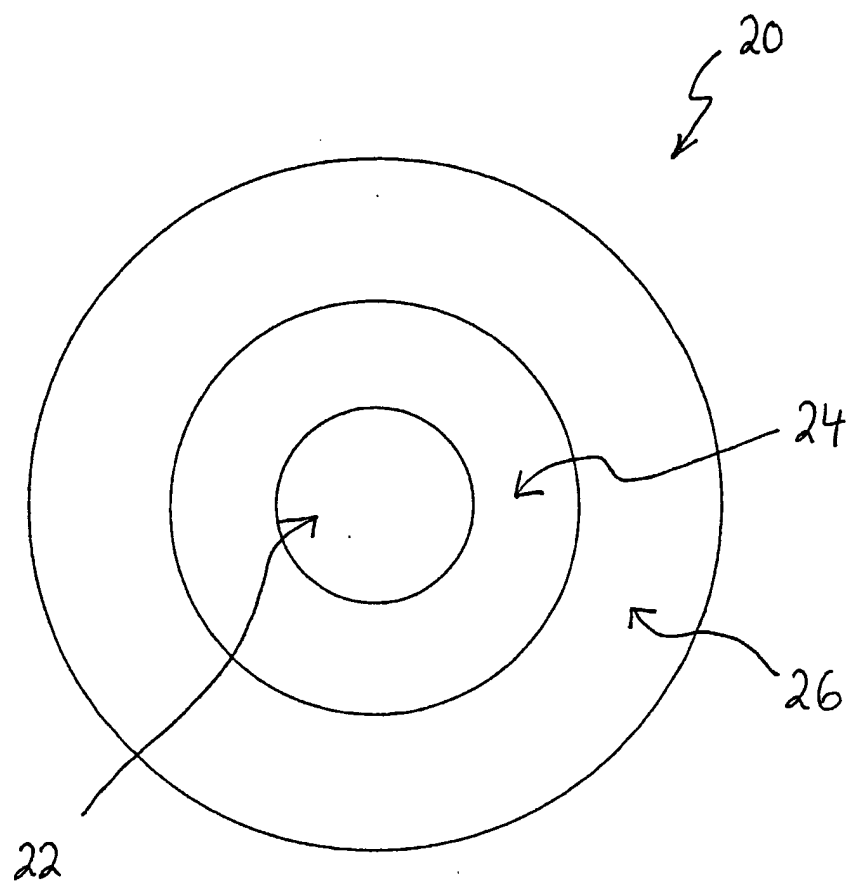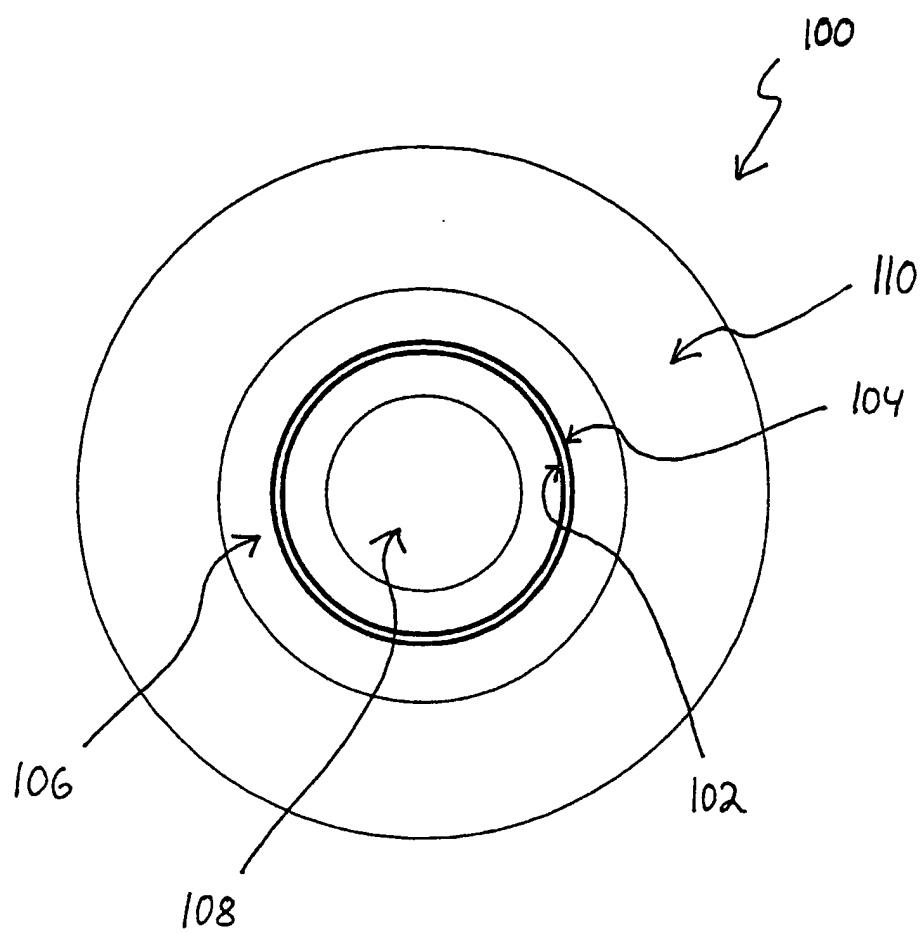
Figure 2

Figure 3

Figure 4

Figure 5

A) 30

34

32

B) 30

36

C) 30 20

Figure 6

TE01

60

70

66

64

20

68

62
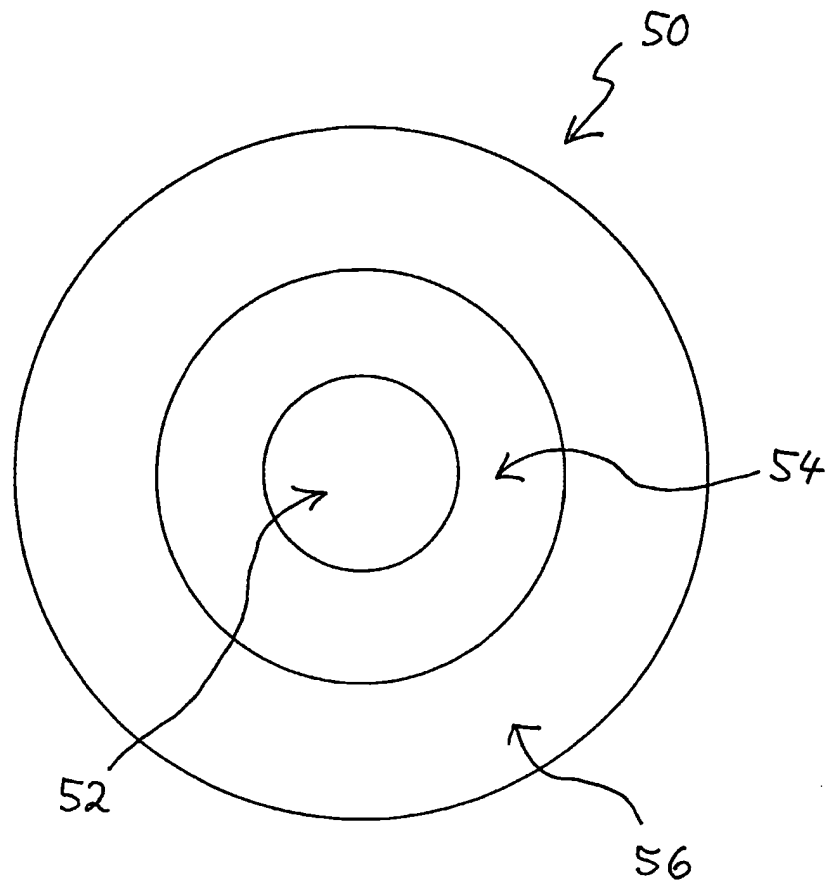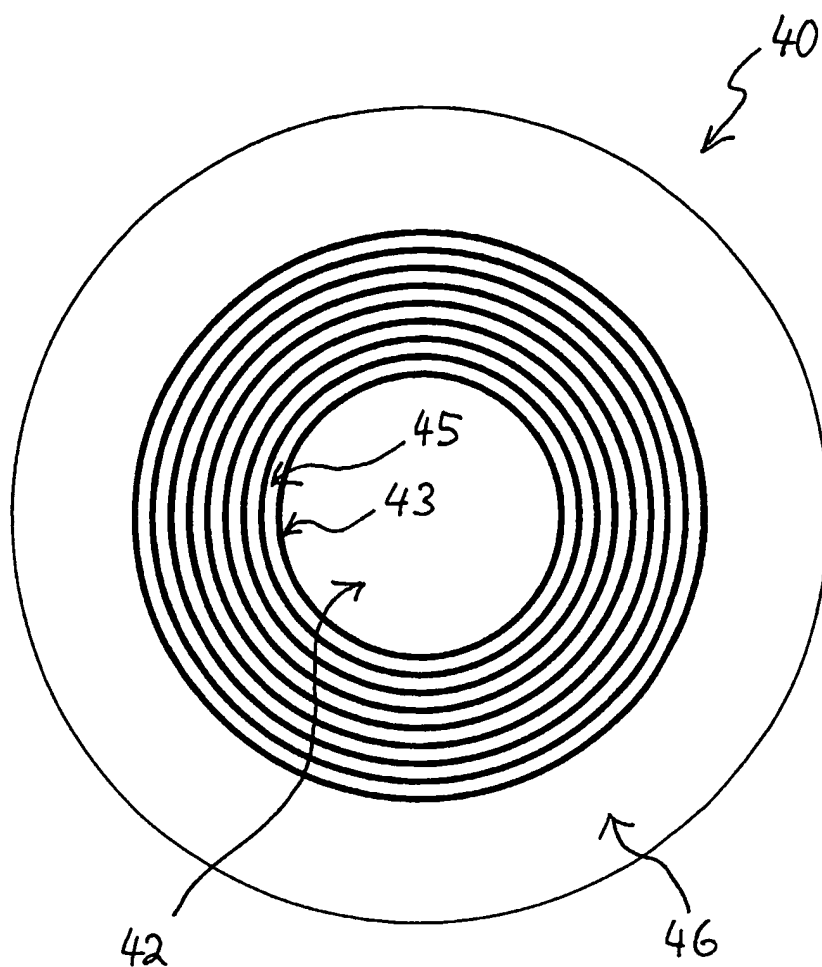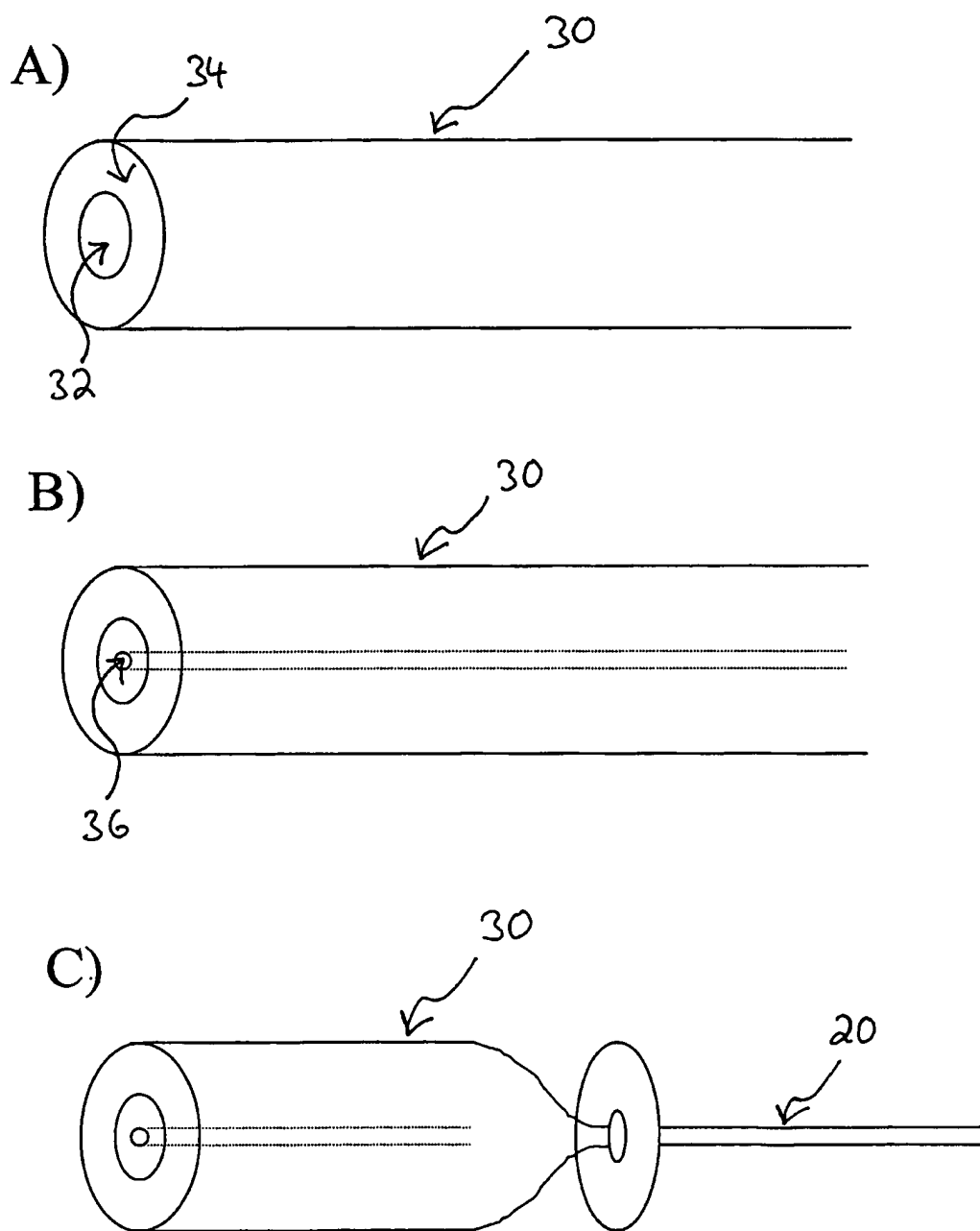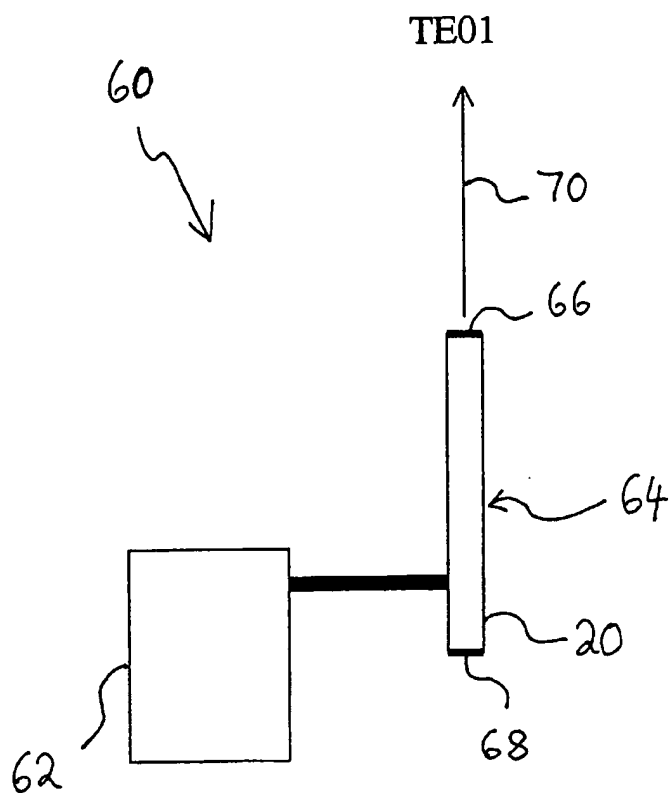
Figure 7

International application No.

PCT/AU02/00435

A.	CLASSIFICATION OF SUBJECT MATTER

Int. Cl. [7]:   G02B 6/16, 6/20, 6/22, 6/34

According to International Patent Classification (IPC) or to both national classification and IPC

B.	FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
REFER TO ELECTRONIC DATABASE BELOW

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
DWPI, JAPIO: G02B 6/-, C03B 37/-, H01S 3/- and keywords [fiber; ring, annular, doughnut; single-mode, mono-mode, non-degenerate mode; hollow, hole; TE01, TEM01; polari+]; keywords only [fiber; index; leak+; mode?]
INSPEC: keywords (fiber; hollow core, low-index core)

C.	DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	OPTICS LETTERS, vol. 25, No. 2, 15 January 2000, BROENG J. et al., "ANALYSIS OF AIR-GUIDING PHOTONIC BANDGAP FIBERS", pp. 96-98 The whole document (in particular, page 98 1st col. lines 19-31)	1-26
A	OPTICS LETTERS, vol. 24, No. 1, 1 January 1999, BARKOU S.E. et al., "SILICA-AIR PHOTONIC CRYSTAL FIBER DESIGN THAT PERMITS WAVEGUIDING BY A TRUE PHOTONIC BANDGAP EFFECT", pp. 46-48 Figures 2, 3 & the corresponding description at pages 47-48	1-26
A	SCIENCE, vol. 285, 3 September 1999, CREGAN R.F. et al., "SINGLE-MODE PHOTONIC BAND GAP GUIDANCE OF LIGHT IN AIR", pp. 1537-1539 Abstract, page 1539 2nd & 3rd cols.	1-26

[X] Further documents are listed in the continuation of Box C	[X] See patent family annex

*	Special categories of cited documents:		
"A"	document defining the general state of the art which is not considered to be of particular relevance	"T"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E"	earlier application or patent but published on or after the international filing date	"X"	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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"O"	document referring to an oral disclosure, use, exhibition or other means	"&"	document member of the same patent family
"P"	document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search	Date of mailing of the international search report
3 June 2002	11 JUN 2002

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C (Continuation).	DOCUMENTS CONSIDERED TO BE RELEVANT	
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 00/49436 A (THE UNIVERSITY OF BATH) 24 August 2000 Page 1 line 17-page 5 line 8, page 16 lines 11-27, figures 6-8	1, 12, 23, 25
A	Patent Abstracts of Japan JP 2000-035521 A (NIPPON TELEGRAPH & TELEPHON CORP) 2 February 2000 Abstract	1-26
A	OPTICS LETTERS, vol. 26, No. 3, 1 February 2001, SHIN Y-I. *et al.*, "DIFFRACTION-LIMITED DARK LASER SPOT PRODUCED BY A HOLLOW OPTICAL FIBER", pp. 119-121 The whole document	1-26
A	US 5056888 A (MESSERLY *et al.*) 15 October 1991 Col. 1 line 18-col. 3 line 12, col. 4 lines 18-47, col. 6 lines 24-32, figs. 1, 4	1, 12, 23, 25

INTERNATIONAL SEARCH REPORT

Information on patent family members

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liabl for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report		Patent Family Member					
WO	200049436	AU	200025650	EP	1153325	AU	200025649
		EP	1153324	WO	200049435		
JP	2000035521	NONE					
US	5056888	AU	58648/90	CA	2020531	EP	414369
		JP	3075607				

END OF ANNEX